



15SW3A 4Ω

The 15SW3A is a high-power 15-inch subwoofer, designed for use in car audio applications. It is specifically designed to reproduce the range of 38 to 150 Hz in a small

The 15SW3A is capable of handling up to 1100 watts RMS (AES or 2200 watts

continuous program power).

A bumped and undercut T-yoke assures a minimum of magnetic rectification (off-centering) and a compatible maximum displacement (Xiim). The extended pole ensure a correct magnetic flux distribution and improve the thermal dissipation The magnet circuit was optimized by finite element software. Special attention was given to the driver's behavior under mechanical overload conditions, meaning that all but the

most severe abuse will be tolerated - without failure.

The 15SW3A employ a 4" (100mm) diameter 4-layer aluminum round wire voice-coil. This is wound on a fiberglass-composite former, twice the thickness of typical formers, to drive the moving assembly with great rigidity.

The pressed-long-fiber-coated pulp cone has the necessary mass and stiffness to withstand the tremendous accelerating forces required, and is precisely centered by

to winstand the tremendous accelerating forces required, and is precisely centered by two counter-balancing, distortion canceling, polyester-cotton-fiber spiders.

A reinforced aluminum frame is highly effective in withstanding mechanical shocks and vibration. It also acts as a heat-sink for the motor, without removing energy from the loudspeakers intended magnetic gap. The aluminum frame includes six vents that allow air exchange between the spider and the top-plate. This helps to reduce top-plate temperature, in turn cooling the voice-coil. The magnetic-circuit also employs a multi-cooling system (natent pending), consisting of a large diameter center hole. multi-cooling system (patent pending) consisting of a large diameter center hole, surrounded by six smaller holes that forces cool air across the voice-coil. These features insure an extremely efficient heat transfer from voice-coil to surroundings, resulting in very high thermal power handling.

SPECIFICATIONS

Nominal diameter	mm (in)
Nominal impedance	Ω
Minimum impedance @ 88.6 Hz 3.63	Ω
Power handling	
Musical program ¹	W
AES ² 1100	W
Sensitivity (2.0V@1m) averaged from 50 to 150 Hz92	dB SPL
Power compression @ 0 dB (nom. power) 2.0	dB
Power compression @ -3 dB (nom. power)/21.3	dB
Power compression @ -10 dB (nom. power)/100.9	dB
Frequency response @ -10 dB 38 to 1,500	Hz

¹ Power handling specifications refer to normal speech and/or music program material, reproduced by an amplifier producing no more than 5% distortion. Power is calculated as true RMS voltage squared divided by the nominal impedance of the loudspeaker.

² AES Standard (60 - 600 Hz).

THIELE-SMALL PARAMETERS

Fs	Hz
Vas	I (ft ³)
Qts	. ,
Qes	
Qms	
ηο (half space)	
Sd	$m^2(in^2)$
Vd (Sd x Xmax)	cm³ (in ³)
Xmax (max. excursion (peak) with 10% distortion) 7.75 (0.30)	mm (in)
Xlim (max.excursion (peak) before physical damage)21.0 (0.83)	mm (in)
Atmospheric conditions at TC necessates magazinements.	
Atmospheric conditions at TS parameter measurements: Temperature 23 (75.2)	°C (°E)

Temperature	*C (*F)
Atmospheric pressure	mb
Humidity	%
•	

Thiele-Small parameters are measured after a 2-hour power test using half AES power . A variation of $\,\pm\,15\%$ is allowed.

ADDITIONAL PARAMETERS

βL	Tm
Flux density	T
Voice coil diameter	mm (in)
Voice coil winding length	m (ft)
Wire temperature coefficient of resistance (α 25)0.00345	1/°C
Maximum voice coil operating temperature 295 (563)	°C (°F)
θvc (max.voice coil operating temp./max.power) 0.27 (0.52)	°C/W(°F/W)
Hvc (voice coil winding depth)	mm (in)
Hag (air gap height)	mm (in)
Re	Ω
Mms	g (lb)
Cms80.0	μm/N
Rms	kg/s
	Ü
NON-LINEAR PARAMETERS	
Le @ Fs (voice coil inductance @ Fs) 5.112	mH
Le @ 1 kHz (voice coil inductance @ 1 kHz) 2.790	mH
Le @ 20 kHz (voice coil inductance @ 20 kHz) 1.529	mH
Red @ Fs	Ω
Red @ 1 kHz	Ω
Red @ 20 kHz	Ω
Krm	Ω
Kxm14.7	mH
Erm	
Evm 0.81	



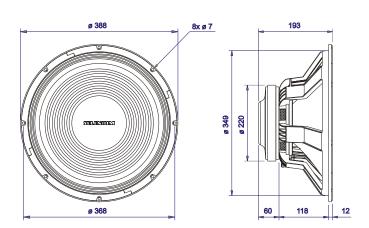
ADDITIONAL INFORMATION

Magnet material	
Magnet weight	3,440 (120) g (oz)
Magnet diameter x depth	220 x 24 (8.66 x 0.95) mm (in)
Magnetic assembly weight	9,350 (20.61) g (lb)
Frame material	
Frame finish	Black epoxy
Voice coil material	Aluminum
Voice coil former material	Fiberglass
Cone material	Pressed long fiber pulp
Volume displaced by woofer	
Net weight	11,040 (24.33) g (lb)
Gross weight	12,260 (28.95) g (lb)
Carton dimensions (W x D x H)48	x 48 x 25 (18.9 x 18.9 x 9.9) cm (in)

MOUNTING INFORMATION

Number of bolt-holes		
Bolt-hole diameter	7.0 (0.27)	mm (in)
Bolt-circle diameter		mm (in)
Baffle cutout diameter (front mount) .	351 (13.81)	mm (in)
Baffle cutout diameter (rear mount)	345 (13.58)	mm (in)
Connectors	Silver-plated p	ush terminals
Polarity	Positive voltage applied t	o the positive

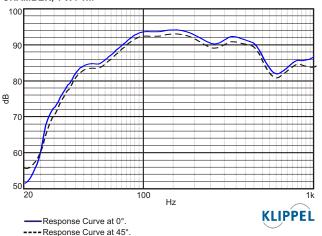
terminal (red) gives forward cone motion





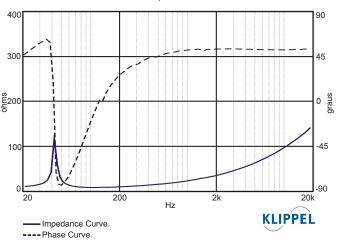
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RESPONSE CURVES (0° AND 45°) IN A TEST ENCLOSURE IN ANECHOIC CHAMBER, 1 W / 1m

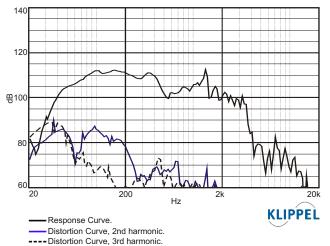


Response curves measured in anechoic chamber with the subwoofer installed in a test enclosure, 1 W / 1 m.

IMPEDANCE AND PHASE CURVES, MEASURED IN FREE-AIR



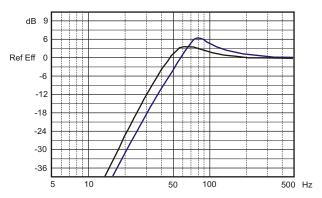
HARMONIC DISTORTION CURVES MEASURED AT 10% AES INPUT POWER IN A TEST ENCLOSURE INSIDE AN ANECHOIC CHAMBER, 1 m



TEST ENCLOSURE

100-liter volume with 3 ducts ø 6" by 7.87" length.

SOFTWARE SIMULATED FREQUENCY RESPONSE CURVE

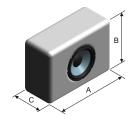


- Curva de Resposta em Closed box 901.
- Curva de Resposta em Closed Box 601.

SUGGESTED ENCLOUSURES				
	CLOSED BOX	VENTED BOX		
TYPE	Internal Volume (Liters)	Internal Volume		Vent (s)
		(Liters)	Qty	Diam. x Length (cm)
15SW3A	XX	90 60	3 3	10 x 06 10 x 05

ENCLOUSURE INTERNAL VOLUME CALCULATION INSTRUCTIONS

TRAPEZOID RECTANGULAR



RECTANGULAR

A x B x (Internal Volume= 1000

Internal Volume: 1000

A, B C and D are internal dimension (in cm). The internal volume result is aiven in liters.

The suggested enclosure volumes are related to only one speaker, including woofer and duct(s) displaced volume.

For enclosure with more than one speaker, it is necessary to multiply the suggested volume and duct(s) by the quantity of speakers and build them with separated chambers (internal division).

Box volumes considering the bass lift inside the car with closed apertures.

HOW TO CHOOSE THE RIGHT AMPLIFIER

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The power amplifier must be able to supply twice the RMS driver power. This 3 dB headroom is necessary to handle the peaks that are common to musical programs. When the amplifier clips those peaks, high distortion arises and this may damage the transducer due to excessive heat. The use of compressors is a good practice to reduce music dynamics to safe levels.

FINDING VOICE COIL TEMPERATURE

It is very important to avoid maximum voice coil temperature. Since moving coil resistance (R_c) varies with temperature according to a well known law, we can calculate the temperature inside the voice coil by measuring the voice coil DC resistance:

$$T_{\rm B} = T_{\rm A} + \left(\frac{R_{\rm B}}{R_{\rm A}} - 1\right) \left(T_{\rm A} - 25 + \frac{1}{\alpha_{25}}\right)$$

 T_A , T_B = voice coil temperatures in °C.

 R_A , R_B voice coil resistances at temperatures T_A and T_B , respectively. $\alpha_{\mbox{\tiny 25}}$ = voice coil wire temperature coefficient at 25 °C.

POWER COMPRESSION

Voice coil resistance rises with temperature, which leads to efficiency reduction. Therefore, if after doubling the applied electric power to the driver we get a 2 dB rise in SPL instead of the expected 3 dB, we can say that power compression equals 1 dB. An efficient cooling system to dissipate voice coil heat is very important to reduce power

NON-LINEAR VOICE COIL PARAMETERS

Due to its close coupling with the magnetic assembly, the voice coil in electrodynamic loudspeakers is a very non-linear circuit. Using the non-linear modeling parameters Krm, Kxm, Erm and Exm from an empirical model, we can calculate voice coil impedance with good accuracy.

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